

ANTENNA PATTERN SYNTHESIS FOR CONFORMAL ARRAYS. COMPARISON OF TWO DIFFERENT METHODS.

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Abstract :

This paper deals with antenna power pattern synthesis in the case of a conformal array of N elements. A lot of synthesis methods have been developed for years but most of them require planar arrays of equispaced elements : one can think of analytical methods such as Schelkounoff, Woodward, Tchebychev,... These techniques are unable to handle conformal arrays. This is why some recent techniques have arisen (see [1] and[2]). Two of them are presented and compared in this paper : the projection method and the variationnal method.

The array factor :

The far-field radiation power pattern of a N sensors array can be written as :

$$f(\mathbf{r}, \theta, \varphi) = \left(\frac{1}{r^2}\right) \cdot \left| \sum_{p=1}^N I_p \cdot f_p(\theta, \varphi) \cdot \exp\left(\frac{2i\pi}{\lambda} \cdot \vec{OM}_p \cdot \vec{u}_r(\theta, \varphi)\right) \right|^2$$

where (r, θ, φ) are the spherical coordinates of the point where the power emitted by the array is measured, λ is the wavelength, \vec{OM}_p is the position of sensor number p, I_p is the complex weight of sensor number p and $f_p(\theta, \varphi)$ is the element number p radiation pattern (in a conformal array, the patterns of the elements point in different directions).

The problem is then to find the N complex weights I_p , such that the function $F(\theta, \varphi) = r^2 \cdot f(r, \theta, \varphi)$ meets a desired pattern defined, for instance, by lower and upper bounds: $G_m(\theta, \varphi) \leq F(\theta, \varphi) \leq G_M(\theta, \varphi)$. These conditions are generally discretized and enforced on M directions (θ_i, φ_i) , with $M \gg N$.

The projection method :

This technique has been introduced in [1] and is based on a iterative two-projections technique.

One builds a (M, N) matrix A and a $(N, 1)$ vector I such that the modulus of the components of AI are the powers $F(\theta, \varphi)$ in the M directions of interest

Step number k > 1:

- 1) if $A \cdot I_k$ meets the desired pattern for the M directions , stop.
- 2) if not, project each component of $A \cdot I_k$ on the (boundary of the) desired pattern and denote the resulting complex vector F^{k+1} .
- 3) the new complex weight vector I_{k+1} is then defined by : $I_{k+1} = \underset{I}{\operatorname{argmin}} \| A \cdot I - F^{k+1} \|$
set $k \rightarrow k + 1$ and return to 1).

The variationnal method :

This technique has been adapted to the pattern synthesis in [2]. It is an iterative fixed point method based on the following criterion function to be minimized :

$$C(I) = \int \int_{\text{side lobes}} |F(\theta, \varphi)|^2 \cdot d\theta \cdot d\varphi + \int \int_{\text{beam}} (G(\theta, \varphi) + |G(\theta, \varphi)|) \cdot d\theta \cdot d\varphi$$

where: $G(\theta, \varphi) = (G_M(\theta, \varphi) - |F(\theta, \varphi)|) \cdot (G_m(\theta, \varphi) - |F(\theta, \varphi)|)$

The conditions for a weight-vector I to be a stationary point of this criterion are then written as a non-linear system of N equations :

$$\mathbf{S} \cdot \mathbf{I} = \mathbf{B}(\mathbf{I})$$

where S is a square N-matrix which does not depend on I.

This system is solved iteratively : $I_{k+1} = (S^\dagger \cdot S)^{-1} \cdot S^\dagger \cdot B(I_k)$ (S^\dagger is the transpose conjugate of S)

Comparison on an example :

These two methods have been used to synthetize the weights to be applied to a circular array (in the $\varphi = 0$ plane) of 32 elements with inter-element spacing $d=0.73 \cdot \lambda$. The desired pattern has side-lobe level lower than $-25dB$ and a main lobe going from $\theta = -30$ deg to $\theta = +30$ deg in the plane $\varphi = 0$ deg.

The two methods allow to find a solution in a few iterations. The variationnal method gives actually lower side-lobe levels than required. Several other examples will be given during the presentation.

References :

- [1] O.M.Bucci, G.Franceschetti, G.Mazzarella, G.Panariello, "Intersection approach to array pattern synthesis", *IEEE Proc.*, vol 137, december 1990.
- [2] C.Audoux, H.Diez, D.Renard, "Synthèse d'antennes réseaux conformées.", *séminaire antennes actives*", pp.212-217, Arles, april 1994.